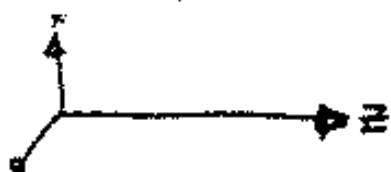


## APPENDIX: EQUATIONS FOR MULTI-LAYER THIN FILM THEORY

IN GENERAL A MONOCHROMATIC PLANE WAVE IN A MEDIUM OF COMPLEX INDEX  $\eta$  WILL HAVE AN ELECTRIC FIELD AMPLITUDE

$$E(z, t) = E(z) e^{i\omega t} \quad \omega = 2\pi f = 2\pi \left( \frac{c}{n\lambda} \right)$$

$$= a \exp \left[ i \left( \omega t - \frac{2\pi}{\lambda} \eta z + \phi_1 \right) \right] + b \exp \left[ i \left( \omega t + \frac{2\pi}{\lambda} \eta z + \phi_2 \right) \right]$$



+z WAVES  
→

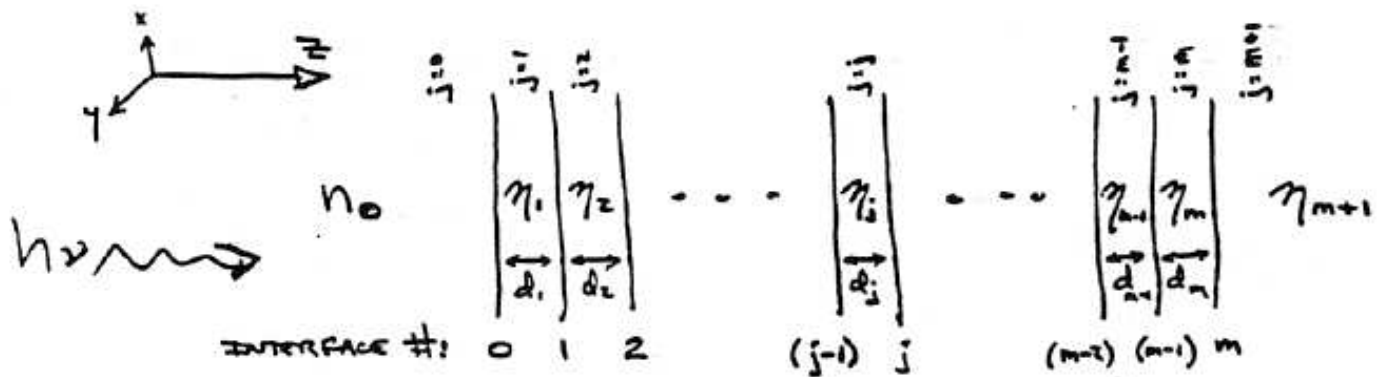
-z WAVES  
←

WHERE  $a, b, \phi_1, \phi_2$  ARE CONSTANTS

TO SPECIALIZE TO THE CASE OF THIN FILMS, ONE DOES TWO THINGS; (1) IMPOSE BOUNDARY CONDITIONS AT EACH INTERFACE WHICH REQUIRE  $E(z, t)$  [AND  $H(z, t)$  AS WELL] TO BE CONTINUOUS, AND (2) CONSIDER ONLY THE TIME AVERAGED BEHAVIOR OF THE AMPLITUDE  $E$ . ONE CAN THEN WRITE A SYSTEM OF EQUATIONS FOR THE  $E_j(z)$  WITHIN EACH LAYER  $j$  AND, IN PRINCIPLE, SOLVE FOR THE CONSTANTS  $a_j, b_j, \phi_{0j}, \phi_{0j}$  OF EACH WAVE TRAIN.

TO SIMPLIFY MATTERS LET ME INTRODUCE THE NOTATION OF P.H. BERNING IN PHYSICS OF THIN FILMS, V. 1 (1963) WHERE THE INTERESTED READER CAN ALSO FIND THE INTERMEDIATE STEPS IN DERIVING RESULTS I ONLY QUOTE HERE

CONSIDER  $m$  LAYERS IN A NON-ABSORBING MEDIUM WITH REFRACTIVE INDEX  $n_0$ , WHICH ARE FOLLOWED BY A MEDIUM OF REFRACTIVE INDEX  $n_{m+1}$ . ASSIGN TO EACH LAYER A SUBSCRIPT " $j$ " AS FOLLOWS



WHERE ALSO LABELLED ARE THE LAYER THICKNESSES AND THE INTERFACES. LIGHT IS INCIDENT FROM THE LEFT. AGAIN, WE HAVE COMPLEX REFRACTIVE INDICES

$$\eta_j = n_j - ik_j$$

NOW AT EACH INTERFACE DENOTE BY A SUPERSCRIPIT ( $t$ )

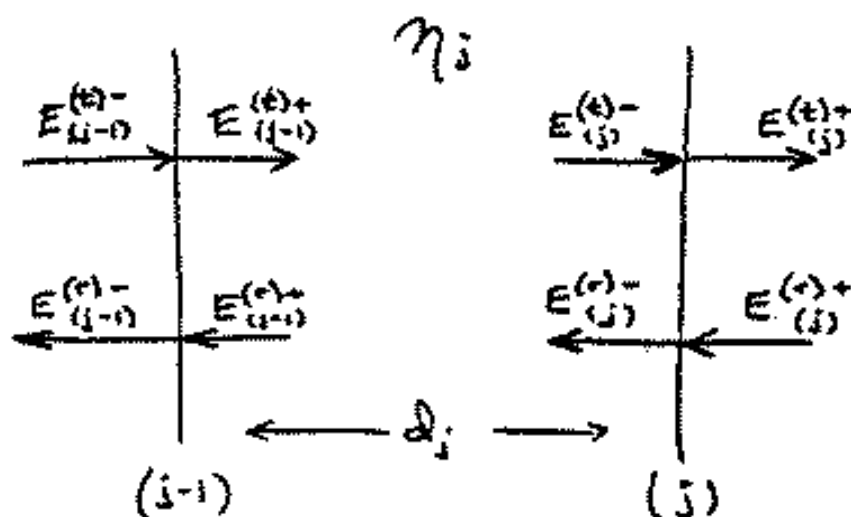
[TRANSMITTED] LIGHT GOING FROM LEFT TO RIGHT AND BY ( $r$ )

[REFLECTED] LIGHT GOING FROM RIGHT TO LEFT. THE ADDITIONAL

SUPERSCRIPIT " $+$ " DENOTES THE RIGHT SIDE OF THE INTERFACE

WHILE " $-$ " DENOTES THE LEFT. HENCE AT INTERFACES

$(j-1)$  AND  $(j)$  ONE HAS ELECTRIC FIELD AMPLITUDES ...



WHERE  $E_{(j-1)}^{(t)-} \neq E_{(j-1)}^{(t)+}$  BECAUSE SOME OF THE INCIDENT ENERGY IS REFLECTED AND CONTRIBUTES THEREFORE TO  $E_{(j-1)}^{(r)-}$ . LIKEWISE  $E_{(j-1)}^{(r)+} \neq E_{(j-1)}^{(r)-}$ , AND THE SAME IS TRUE AT INTERFACE (j).

HOWEVER, IT IS POSSIBLE TO WRITE OUR SYSTEM OF EQUATIONS IN THIS NOTATION AND DERIVE RELATIONS BETWEEN THESE AMPLITUDES. THE BOUNDARY CONDITIONS REQUIRE OF COURSE THAT

$$E_{(j)}^{(t)-} + E_{(j)}^{(r)-} = E_{(j)}^{(t)+} + E_{(j)}^{(r)+}$$

$$\text{AND } \eta_j [E_{(j)}^{(t)-} - E_{(j)}^{(r)-}] = \eta_{j+1} [E_{(j)}^{(t)+} - E_{(j)}^{(r)+}]$$

$$\text{ALSO NOTE: } E_{(j-1)}^{(t)+} = E_{(j)}^{(t)-} \exp \left[ i \left( \frac{2\pi}{\lambda} \eta_j d_j \right) \right]$$

$$\text{AND } E_{(j-1)}^{(r)+} = E_{(j)}^{(r)-} \exp \left[ -i \left( \frac{2\pi}{\lambda} \eta_j d_j \right) \right]$$

FOR SIMPLICITY DEFINE  $\Phi_j = \left( \frac{2\pi}{\lambda} \eta_j d_j \right)$ .

COMBINING THESE RELATIONS ONE CAN RELATE THE AMPLITUDES AT INTERFACE  $(j-1)$  TO THOSE AT  $(j)$  AS FOLLOWS ...

$$E_{(j-1)}^{(+)} = \frac{1}{2} \left( 1 + \frac{\eta_j}{\eta_{j-1}} \right) E_{(j)}^{(+)} \exp[i\Phi_j] + \frac{1}{2} \left( 1 - \frac{\eta_j}{\eta_{j-1}} \right) E_{(j)}^{(-)} \exp[-i\Phi_j]$$

AND LIKEWISE

$$E_{(j-1)}^{(-)} = \frac{1}{2} \left( 1 - \frac{\eta_j}{\eta_{j-1}} \right) E_{(j)}^{(+)} \exp[i\Phi_j] + \frac{1}{2} \left( 1 + \frac{\eta_j}{\eta_{j-1}} \right) E_{(j)}^{(-)} \exp[-i\Phi_j]$$

SO THAT THE COMPUTER CAN SOLVE FOR THE ELECTRIC FIELD AMPLITUDES RECURSIVELY (AND IT'S GOOD AT THAT!).

THIS RECURSIVE SOLUTION MUST START AT THE  $m$ -th INTERFACE BECAUSE ONLY THERE DO WE HAVE THE ADVANTAGE OF KNOWING THAT  $E_{(m)}^{(+)} = 0$  ... NO LIGHT IS INCIDENT UPON THE LAST INTERFACE FROM THE RIGHT.  $E_{(m)}^{(+)}$  CAN BE SET = 1 AS A START AND ALL AMPLITUDES AND PHASES REFERENCED TO IT GOING FROM RIGHT TO LEFT UNTIL REACHING  $j=0$ .

WITH ALL THE  $E_{(j)}^{(+)}$  KNOWN, IT IS NOW A SIMPLE MATTER TO CALCULATE THE REFLECTION, TRANSMISSION, AND ABSORPTION OF THE LAYERS AS FOLLOWS ...

$$R = \left| \frac{E_0^{(+)} - E_0^{(-)}}{E_0^{(+)} + E_0^{(-)}} \right|^2$$

$$T = \frac{\text{Re}\{\eta_{m+1}\}}{n_0} \left| \frac{E_m^{(+)} + E_0^{(-)}}{E_0^{(+)} + E_0^{(-)}} \right|^2$$

AND FOR THE ABSORPTION IN THE  $j^{\text{th}}$  LAYER ...

$$A_j = \frac{\text{Re}\{\eta_j\} \left[ |E_{(j-1)}^{(+)}|^2 - |E_{(j-1)}^{(-)}|^2 - |E_{(j)}^{(+)}|^2 + |E_{(j)}^{(-)}|^2 \right]}{n_0 |E_0^{(+)}|^2}$$

$$= \frac{2 \text{Im}\{\eta_j\} \left[ \text{Im} \left( E_{(j-1)}^{(+)} E_{(j-1)}^{(+)*} \right) - \text{Im} \left( E_{(j)}^{(+)} E_{(j)}^{(+)*} \right) \right]}{n_0 |E_0^{(+)}|^2}$$

WITH NATURALY GIVES

$$R + T + \sum_j A_j = 1$$

**LORAL**

Fairchild Imaging Sensors

## CCD412

### 512 x 512 Element Full Frame Image Sensor

**FEATURES**

- 512 x 512 Photosite Array
- 15 $\mu$ m x 15 $\mu$ m Pixel
- 7.68mm x 7.68mm Image Area
- 100% Fill Factor
- Multi-Pinned Phase (MPP) Option
- Readout Noise Less Than 7 Electrons
- Dynamic Range 10,000:1
- Single Output Channel
- Three Phase Buried Channel NMOS

**GENERAL DESCRIPTION**

The CCD412 is a 512 x 512 element solid state Charge Coupled Device (CCD) Full Frame area image sensor which is intended for use in high resolution scientific, industrial, and commercial electro-optical systems. The CCD412 is organized as a matrix array of 512 horizontal by 512 vertical CCD photosites. The pixel pitch and spacing is 15 $\mu$ m.

The imaging array may be operated in one of three modes, Buried Channel, Multi-Pinned Phase (MPP), and Surface Channel. The Buried Channel operation offers low noise performance and excellent charge transfer efficiencies. An additional implant under one vertical phase creates a virtual well which collects the photo-electrons with all Vertical clocks low during integration. This MPP mode decreases dark current down to 25 pA/cm<sup>2</sup> @ 25°C. The CCD412 may be operated in a Surface Channel mode, to increase full well capacity.

Excellent low noise performance is achieved by use of the buried channel CCD structure and a single stage low noise output amplifier.

Device processing is done using 2.5 micron design rules. The single metal, triple-poly process allows a photosite layout with smaller pixel geometries and fewer array finishes.

**FUNCTIONAL DESCRIPTION**

The CCD412 consists of the following functional elements illustrated in the block diagram.

**Image Sensing Elements:** Incident photons pass through a transparent polycrystalline silicon gate structure and are absorbed in the silicon crystal structure creating electron hole pairs. The resulting photo-electrons are collected in the photosites during the integration period. The amount of charge accumulated in each photosite is a linear function of the localized incident illumination intensity and integration period.

The photosite structure is made up of contiguous CCD elements with no voids or inactive areas. In addition to sensing light, these elements are used to shift image data vertically. Consequently, the device needs to be covered during readout.

**Vertical Charge Shifting:** The Full Frame architecture of the CCD412 provides video information as a single sequential

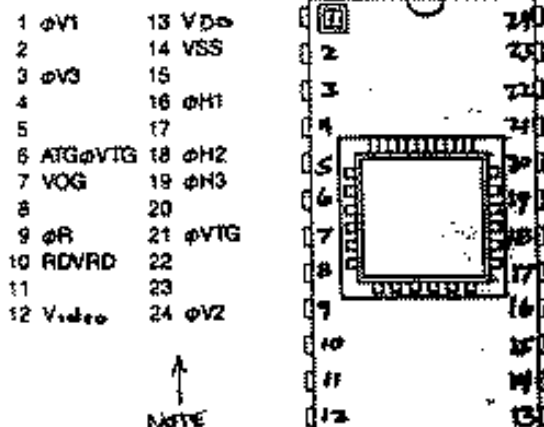


readout of 512 lines containing 512 photosite elements. At the end of an integration period the  $\phi V_1$ ,  $\phi V_2$ , and  $\phi V_3$  clocks are used to transfer charge vertically through the CCD array to the horizontal readout registers. Vertical columns are separated by a channel stop region to prevent charge migration.

The Vertical Transfer Gate (VTG) is the final array gate before charge is transferred to the serial horizontal shift registers. Simplified operation  $\phi$ VTG may be tied to  $\phi V_2$ .

**Horizontal Charge Shifting:**  $\phi H_1$ ,  $\phi H_2$ , and  $\phi H_3$  are polysilicon gates used to transfer charge horizontally to the output amplifier. The horizontal transport register is twice the size of the photosite to allow for vertical binning. With binning an array can be operated normally at full resolution, as a 256 x 512, 256 x 256, or some other resolution.

PIN NUMBER/NAME	PIN CONNECTIONS
1 $\phi V_1$	13 VDD
2	14 VSS
3 $\phi V_3$	15
4	16 $\phi H_1$
5	17
6 ATG $\phi$ VTG	18 $\phi H_2$
7 VOG	19 $\phi H_3$
8	20
9 $\phi R$	21 $\phi$ VTG
10 RDVRD	22
11	23
12 Video	24 $\phi V_2$



NOTE  
THIS COLUMN  
INVERTED (ACTUALLY)

