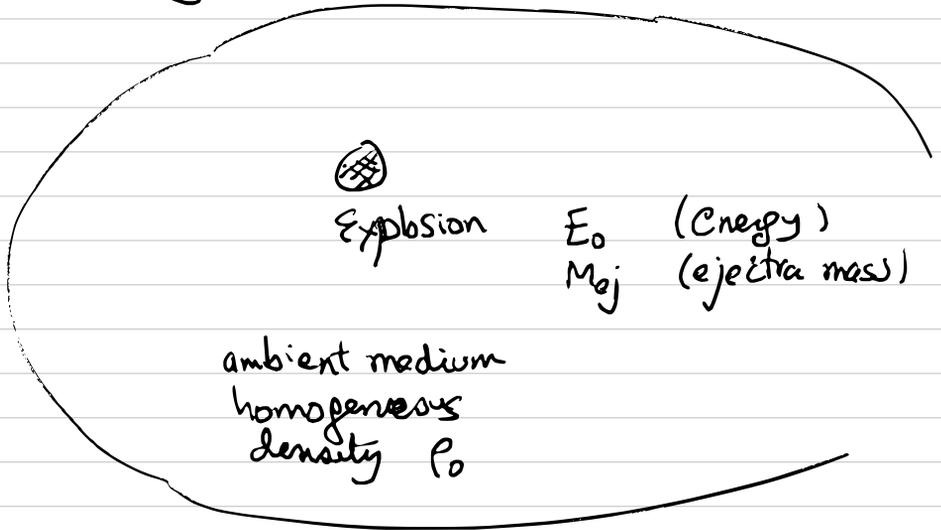


Sedov-Taylor solution

DRAINE, ch 39



Stage 1: Free expansion.

Ejecta expands at velocity, v_{rms}

$$\frac{1}{2} M_{ej} v_{rms}^2 = E_0$$

$$v_{rms} \approx \left(\frac{2E_0}{M_{ej}} \right)^{1/2}$$

For Supernovae

$$E_0 = 10^{51} \text{ erg ("foe", Bethe)}$$

M_{ej} ... normalized to M_\odot

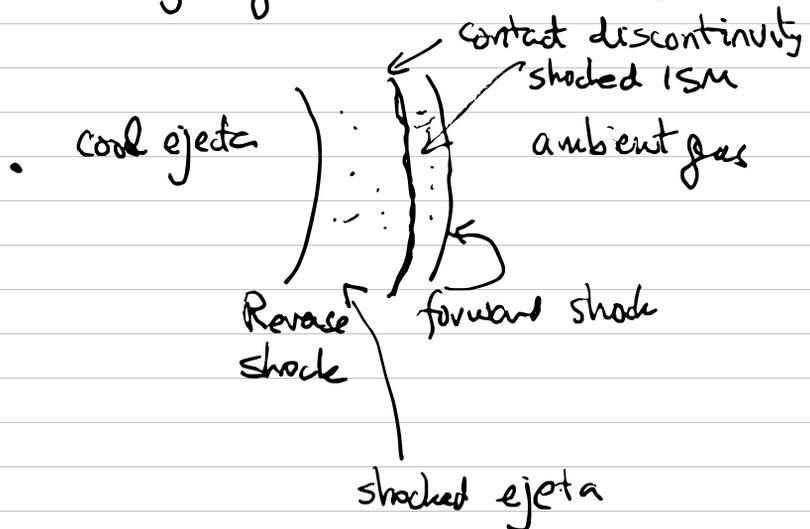
$$v_{rms} = 10^4 \text{ km/s } E_{51}^{1/2} \left(\frac{M_{ej}}{M_\odot} \right)^{-1/2}$$

As ejecta ballistically expands the ~~dens~~ mean density of ejecta falls as t^{-3}

The ejecta cools rapidly ($PV^\gamma = \text{constant}$)

Once the ram pressure, $\rho(t)v_{\text{rms}}^2$ approaches mean ambient pressure, P_{amb} , a "reverse" shock sets in.

[The leading edge of ejecta slows down.
The trailing edge starts to catch up]



Radius r at which ρ reverse shock reaches the center

$$R_1 = (3Me) / (4\pi\rho_0) \approx$$

$$R_1 \approx 2 \text{ pc} \left(\frac{M_{ej}}{M_\odot} \right)^{1/3} n_0^{-1/3} \dots$$

↑
atoms/cm³

Corresponding to epoch

$$t_1 \approx \frac{R_1}{v_{rms}} = 186 \text{ yr} \left(\frac{M_{ej}}{M_\odot} \right)^{5/6} E_{51}^{-1/3} n_0^{-1/3}$$

Stage 2: Sedov-Taylor.

The ejecta is now heated, again

Similarity analysis:

This is a more powerful approach compared to dimensional analysis

The free parameters are

$$E_0, \rho_0$$

(M_{ej} has disappeared since $M_{\text{swept-up}} \gg M_{ej}$)

Step 1: Dimensional analysis

$$R_s = A E^\alpha \rho^\beta t^\gamma$$

↑
radius of shock front

With modest effort

$$R_s = \xi E^{1/5} \rho_0^{-1/5} t^{2/5}$$

Surprisingly with a lot of handwork

$$\xi \approx 1.15167 \quad (!)$$

$$R_s \approx 5 \rho_0 \left(\frac{E s_1}{n_0} \right)^{1/5} t_3^{2/5}$$

↑
10³ yr

$$V_s \approx 1950 \text{ km/s} \left(\frac{E s_1}{n_0} \right)^{1/5} t_3^{-3/5}$$

$$T_s = 5.2 \times 10^7 \text{ K} \left(\frac{E}{n_0} \right)^{2/5} t_3^{-6/5}$$

↑
obtained using shock jump equations

Step 2:

Similarity analysis

$$\rho(r) = \rho_0 f(x) \quad x = \frac{r}{R_s}$$

$$v(r) = \frac{R_s}{t} g(x)$$

$$p(r) = \frac{\rho_0 R_s^2}{t^2} h(x)$$

↑ sensible choices

Sedov-Taylor formulation:

Shu, Volume II, Ch 17

$$\rho_2 = \left(\frac{\gamma+1}{\gamma-1} \right) \rho_1$$

Strong-shock jump conditions:

$$u_2 = \left(\frac{2}{\gamma+1} \right) v_s$$

$$P_2 = \frac{2}{(\gamma+1)} \rho_1 v_s^2$$

The equations

$$(1) \quad \frac{\partial \rho}{\partial t} + \frac{1}{r^2} \frac{\partial}{\partial r} (r^2 \rho u) = 0$$

$$(2) \quad \frac{\partial u}{\partial t} + u \frac{\partial u}{\partial r} = - \frac{1}{\rho} \frac{dP}{dr}$$

$$(3) \quad \frac{\partial}{\partial t} \left[\rho \left(\mathcal{E} + \frac{1}{2} u^2 \right) \right] + \frac{1}{r^2} \frac{\partial}{\partial r} \left[r^2 \rho u \left(\mathcal{E} + \frac{P}{\rho} + \frac{1}{2} u^2 \right) \right] = 0$$

$$\mathcal{E} = \left(\frac{P}{\rho} \right) \frac{1}{\gamma-1}$$

We now apply self-similarity expectations

$$P(r, t) = \left(\frac{\gamma+1}{\gamma-1}\right) P_1 \alpha\left(\frac{r}{R_s}\right) = P_2 \alpha\left(\frac{r}{R_s}\right)$$

$$U(r, t) = \frac{4}{5(\gamma+1)} \frac{r}{t} v\left(\frac{r}{R_s}\right) = U_2 \frac{r}{R_s} v\left(\frac{r}{R_s}\right)$$

$$P(r, t) = \frac{8}{25(\gamma+1)} P_1 \left(\frac{r}{t}\right)^2 p\left(\frac{r}{R_s}\right) = P_2 \left(\frac{r}{R_s}\right)^2 p\left(\frac{r}{R_s}\right)$$

Substitute these into (1)-(3).

Solve numerically (Taylor) or analytically (Sedov.)

In the Sedov-Taylor phase the interior is hot. \Rightarrow very little radiative loss.

As shock speed falls, cooling increases

ST ends, say when, $AE/E_0 \approx -1/3$

$$t_{\text{end}} = 5 \times 10^4 \text{ yr } E_{51}^{0.22} n_0^{-0.55}$$

$$R_{\text{end}} = 24 \text{ pc } E_{51}^{0.29} n_0^{-0.42}$$

$$V_s = 188 \text{ km/s } (E_{51} n_0)^{0.07}$$

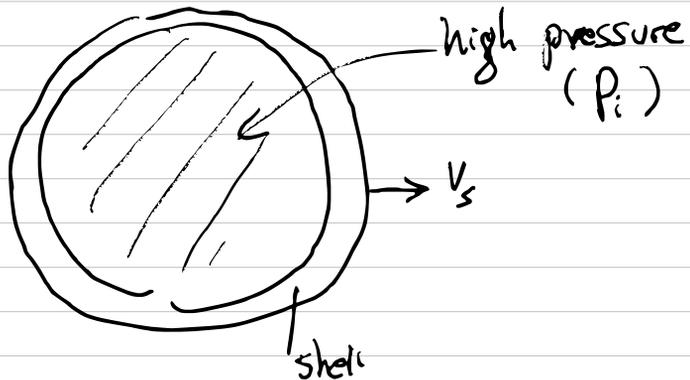
$$kT_s \approx 41 \text{ eV } (E_{51} n_0^2)^{0.13}$$

Stage 3: Snow-plow phase

The post-shocked gas cools strongly

(recall $v_{\text{shock}} \approx 188 \text{ km/s}$ at the start of this phase)

The post-shock gas collapses to a high density shell.



The hot interior drives the shell outward

$$P V^\gamma = \text{constant} \quad \gamma = 5/3$$
$$V \propto R^3$$

$$P_i = P_o(t=t_{\text{rad}}) \left(\frac{R_{\text{rad}}}{R_s} \right)^5$$

\nwarrow interior

$$t_{\text{rad}} = 49 \times 10^3 E_{51}^{0.22} n_0^{-0.55} \text{ yr}$$
$$R_{\text{rad}} = 7.3 \times 10^{19} \text{ cm } E_{51}^{0.29} n_0^{-0.42}$$

The force equation is

$$\begin{aligned}\frac{d}{dt}(M_s v_s) &= p_i 4\pi R_s^2 \\ &= 4\pi p_0 (t = t_{\text{rad}}) R_{\text{rad}}^5 R_s^{-3}\end{aligned}$$

Note $v_s = \frac{dR_s}{dt}$

$$\dot{M}_s = R_s^2 v_s = R_s^2 \dot{R}_s$$

Assume

$$R_s \propto t^\eta$$

$$\Rightarrow \dot{M}_s \propto t^{3\eta-1}$$

$$\Rightarrow M_s \propto t^{3\eta}$$

$$\therefore \frac{d}{dt}(M_s \dot{R}_s) \propto t^{4\eta-2} \propto R_s^{-3}$$

$$\therefore \eta = 2/7$$

In "snowplow" phase $R_s \propto \left(\frac{t}{t_{\text{rad}}}\right)^{2/7}$

$$v_s = \frac{2}{7} \frac{R_s(t_{\text{rad}})}{t_{\text{rad}}} \left(\frac{t}{t_{\text{rad}}}\right)^{-5/7}$$

Stage 4: Fade-out.

(Dumps remaining kinetic energy into the ISM)